



Seismic Performance of Stainless Steel-Reinforced Concrete Piers: Experimental & Numerical

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1 Background



- *The Cost of Corrosion in China* was released in 2017
- The corrosion cost for highway bridges reached **¥62.47 billion** in 2014



- **Maintenance costs for existing bridges** could reach up to **\$125 billion**
- An **annual budget** of **\$22.7 billion** is required to improve structurally deficient bridges



Stonecutters Bridge
(2009)



Hong Kong-Zhuhai-Macao Bridge
(2018)



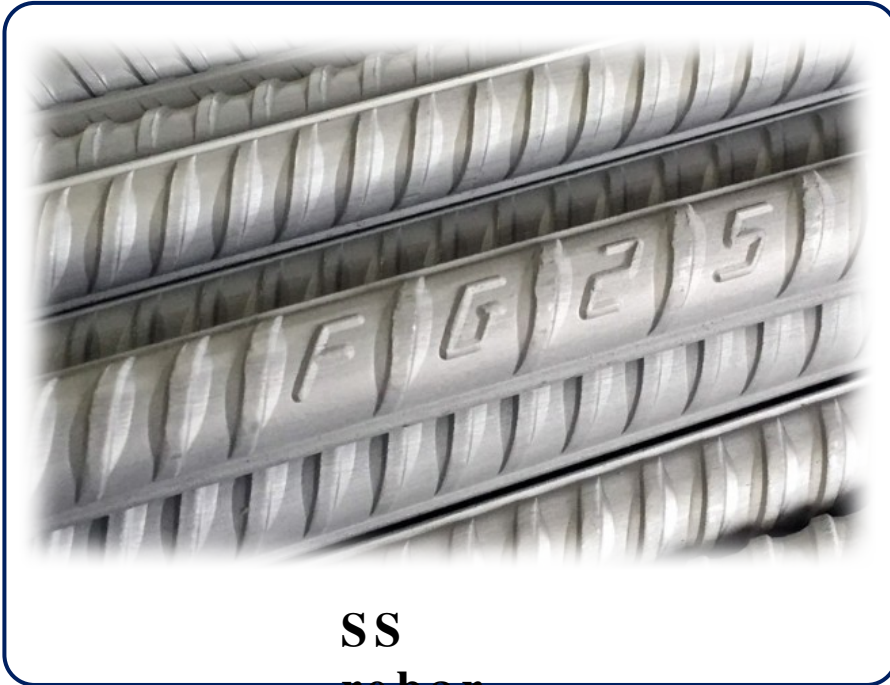
Champlain Bridge
(2019)

- In recent years, **stainless steel reinforcement bars** have been widely adopted in coastal and cross-sea bridges to solve **durability issues**.

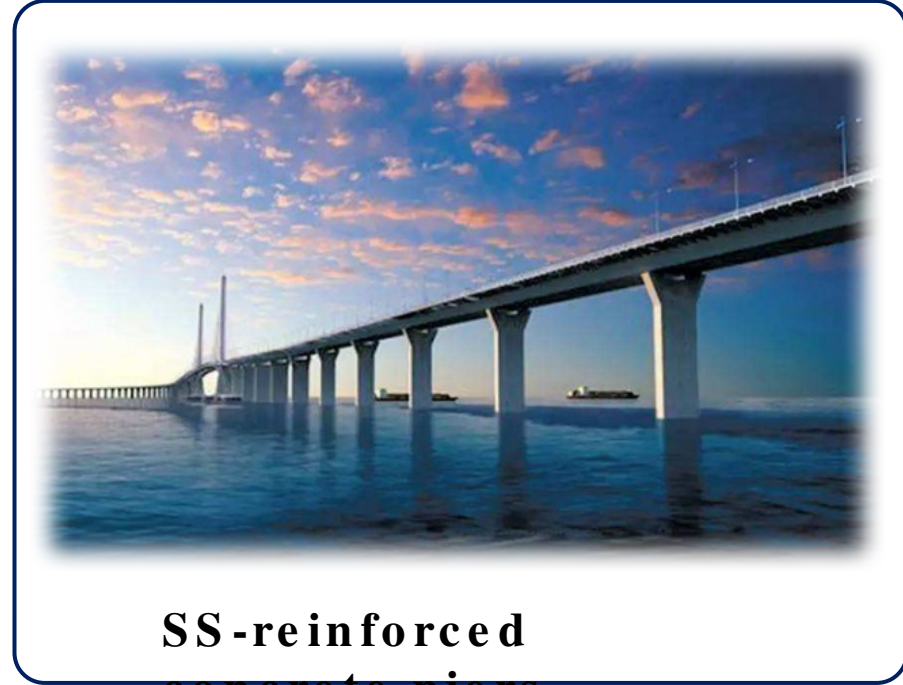
1 Background

SS Reinforcement Bars:

- ✓ Corrosion resistance ✓ High strength ✓ Durability ✓ Low maintenance
- ✓ High-temperature resistance ✓ Fatigue resistance



**SS
rebar**

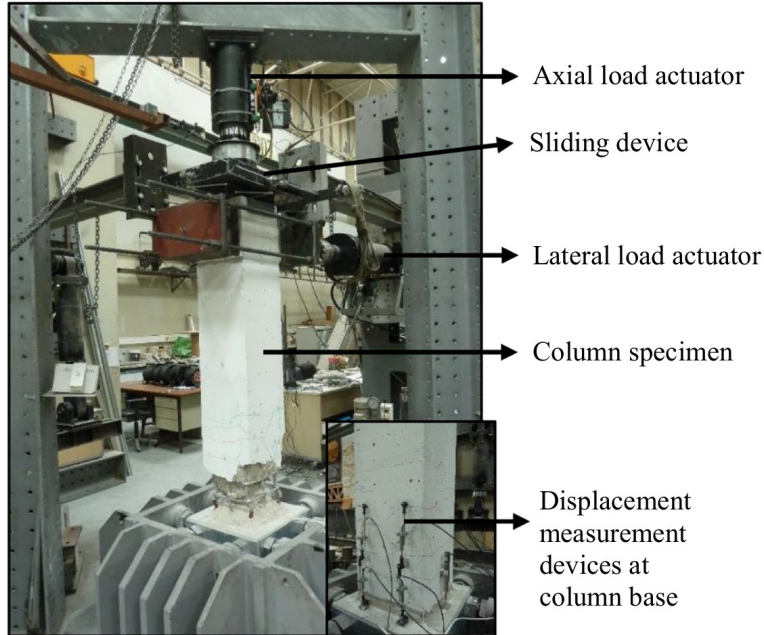


**SS-reinforced
concrete piers**

SS-Reinforced Concrete Bridges:

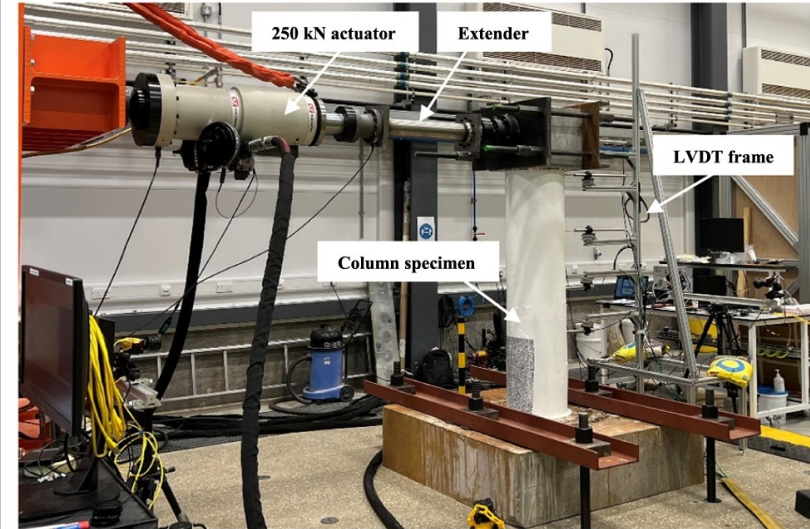
- ✓ Exceptional corrosion resistance ✓ Long service life ✓ Low maintenance costs ✓ High strength and toughness ✓ Eco-friendly sustainability ✓ Special environmental adaptability

1 Background



Melo et al. (2022)

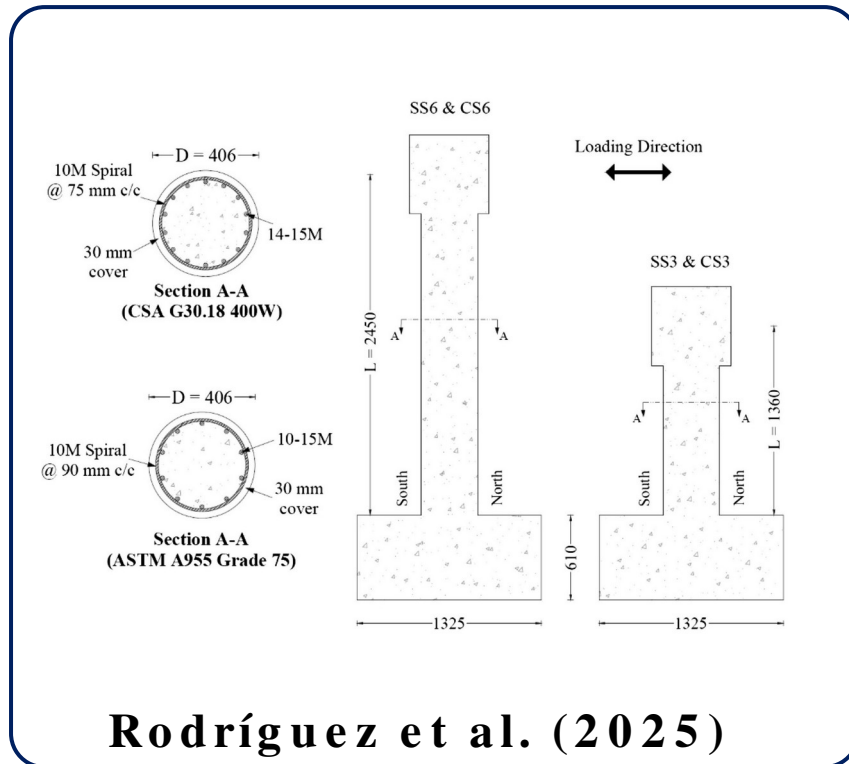
- 3 specimens with height of **1.65 m**
- 1.4462 **duplex** stainless steel rebars
- **Pushover** and **quasi-static** tests
- Higher **ultimate strength**
- Better **deformation capacity**



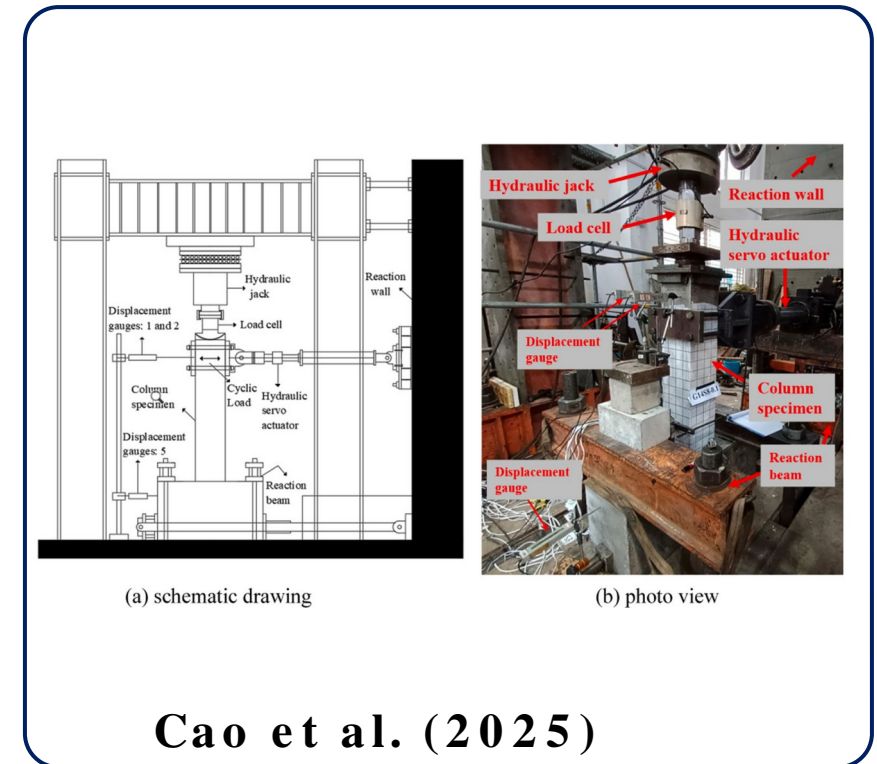
Moodley et al. (2024)

- 3 specimens with height of **2.00 m**
- **Duplex** & **austenitic** stainless rebars
- Larger **yield displacement**
- Higher **ultimate strength**
- Better **deformation capacity**

1 Background



- 4 specimens with height of **2.45 m**
- ASTM A955 Grade 75 **SS rebar**
- **Slender ratio** of 3 & 6
- Higher **ultimate strength**
- **Buckling** of SS



- **Hybrid reinforcement** of SS and GFRP
- **Axial ratio** & **hybrid reinforcement ratio**
- Better **deformation capacity**
- Increasing **energy dissipation capacity**

1 Background

- Research on the SSRC piers **remains limited** at present.
- Current **codes and standards lack specific provisions** for the seismic design.
- Significant research potential persists across **material properties**, **component behaviour**, and **structural system** performance of SSRC piers.



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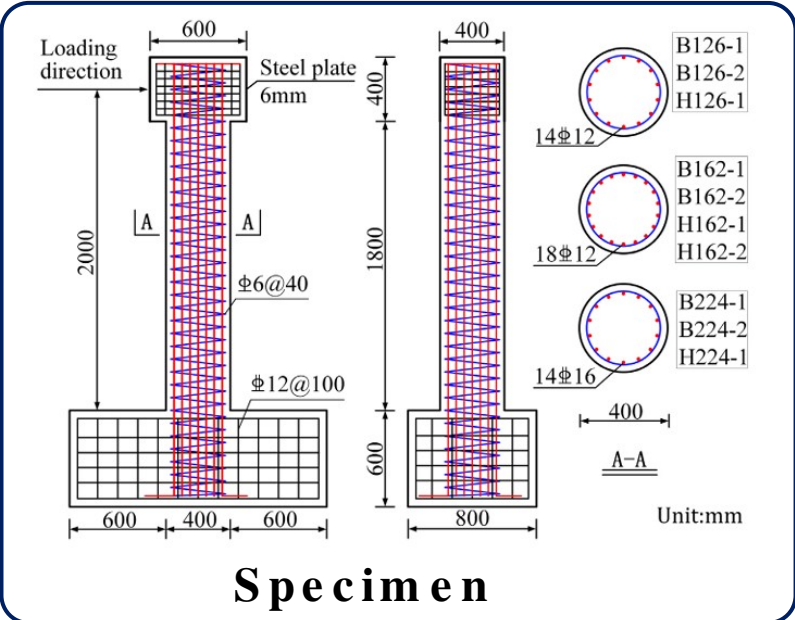
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2 Quasi-static tests of SS-reinforced piers

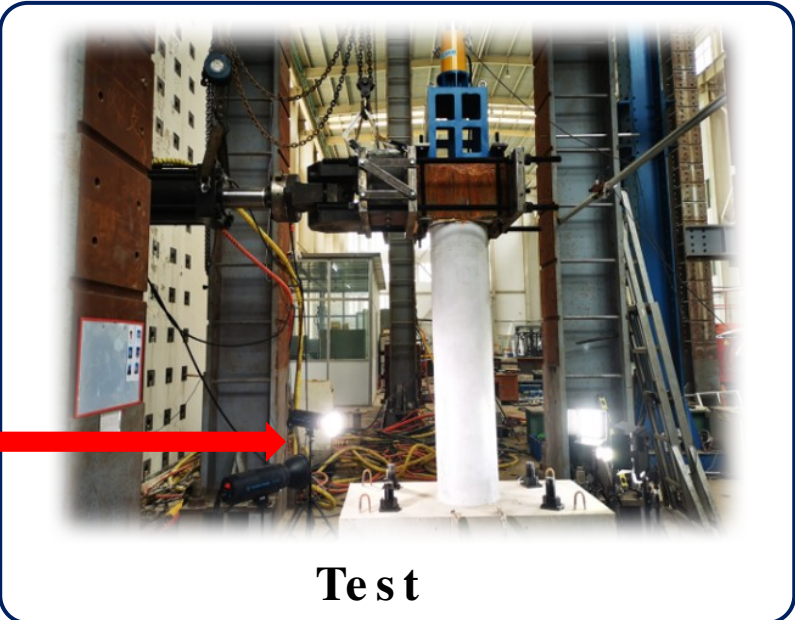


Specimen design

- 10 specimens
- 2m tall
- C55 concrete



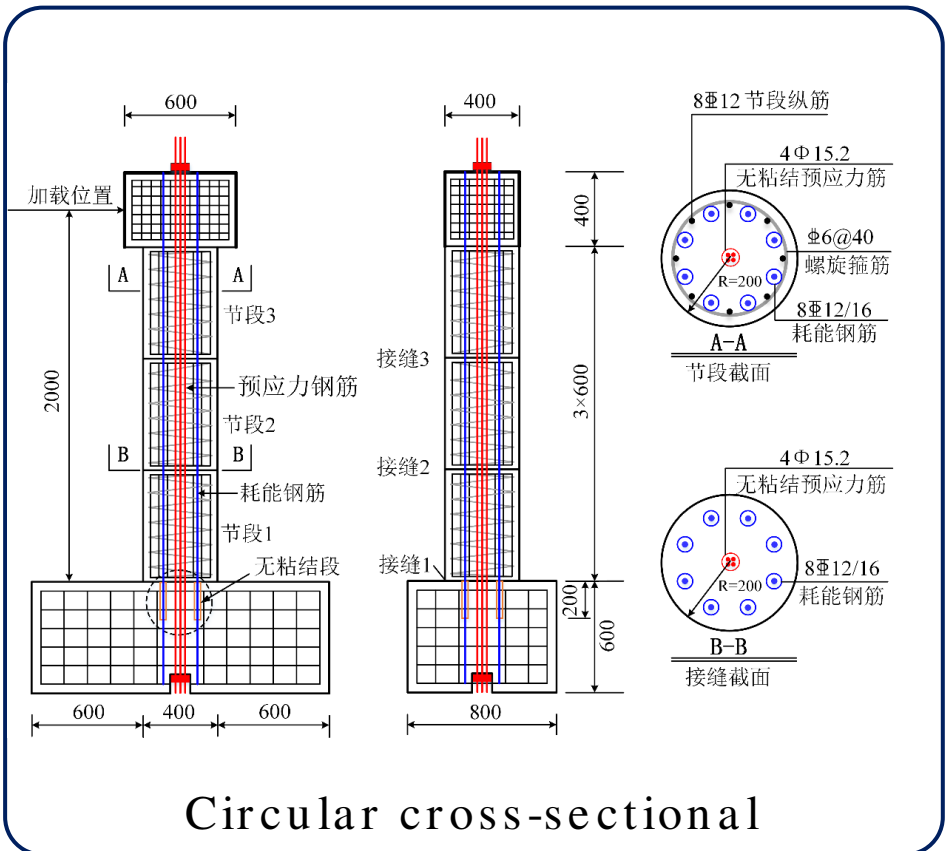
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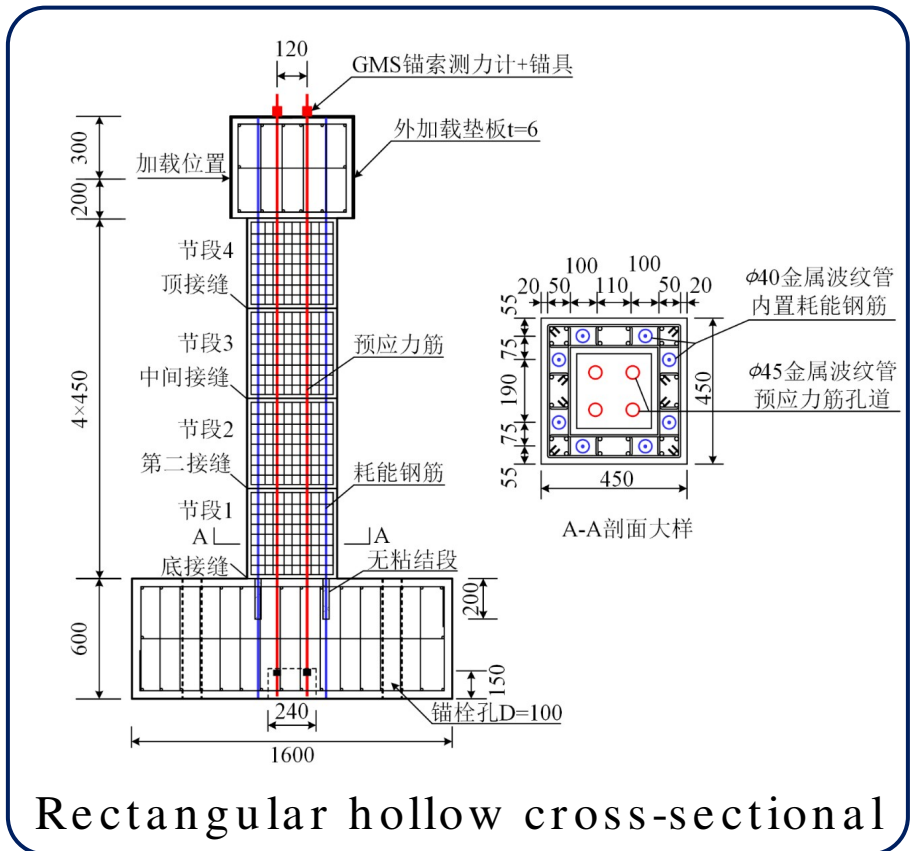
Test setup

Specimen	Reinforcement parameters				Axial load		
	Vertical bar	Reinforcement ratio ρ (%)	Rebar type	Spiral			η
	Diameter			Diameter	ρ (%)	Type	
B126-01	14D12	1.26	B1.4362	C6@40mm	1.0	B1.4362	0.1
B126-02	14D12	1.26	B1.4362	C6@40mm	1.0	B1.4362	0.2
B162-01	18D12	1.62	B1.4362	C6@40mm	1.0	B1.4362	0.1
B162-02	18D12	1.62	B1.4362	C6@40mm	1.0	B1.4362	0.2
B224-01	14D16	2.24	B1.4362	C6@40mm	1.0	B1.4362	0.1
B224-02	14D16	2.24	B1.4362	C6@40mm	1.0	B1.4362	0.2
H126-01	14D12	1.26	HRB500	C6@40mm	1.0	HRB400	0.1
H162-02	18D12	1.62	HRB500	C6@40mm	1.0	HRB400	0.2
H162-01	18D12	1.62	HRB500	C6@40mm	1.0	HRB400	0.1
H224-02	14D16	2.24	HRB500	C6@40mm	1.0	HRB400	0.2

2 Quasi-static tests of SS-reinforced piers



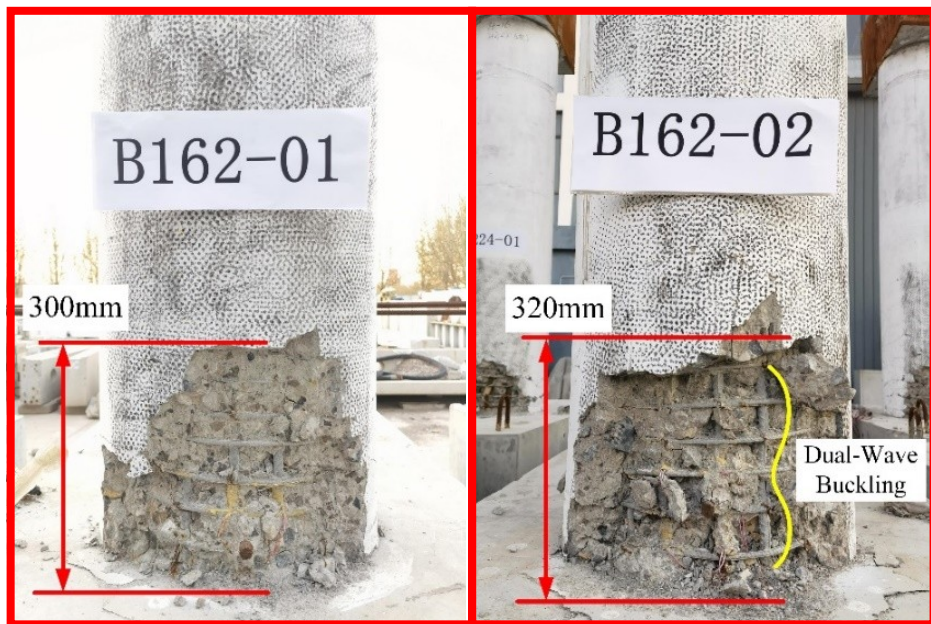
Circular cross-sectional specimens



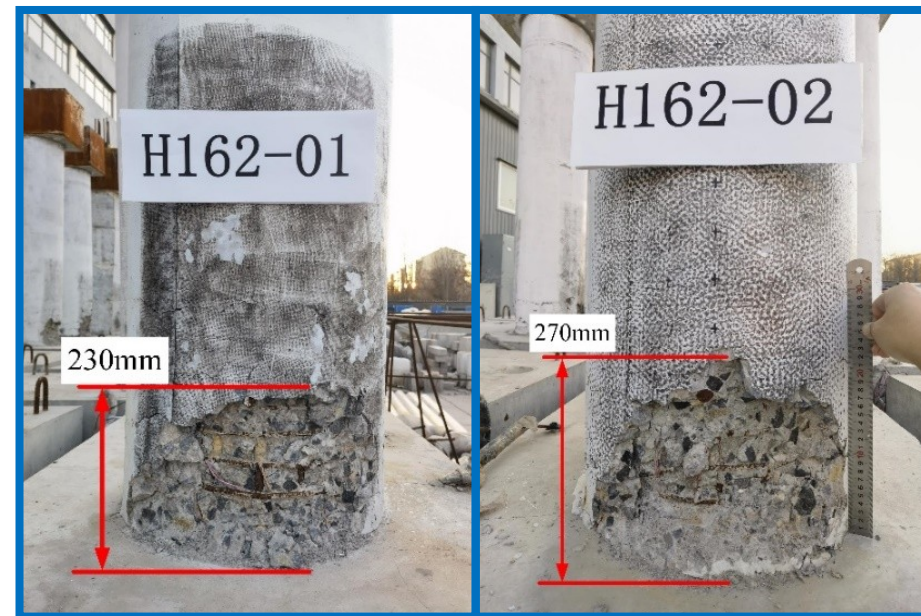
Rectangular hollow cross-sectional specimens

Completed quasi-static tests on **prestressed segmental piers** with **SS energy-dissipating bars** (total: 15 specimens)

- 7 **circular** cross-section prefabricated bridge piers
- 8 **rectangular hollow** cross-section prefabricated bridge piers



SS-reinforced pier
Reinforcement ratio: 1.62 %,
axial load: 0.2

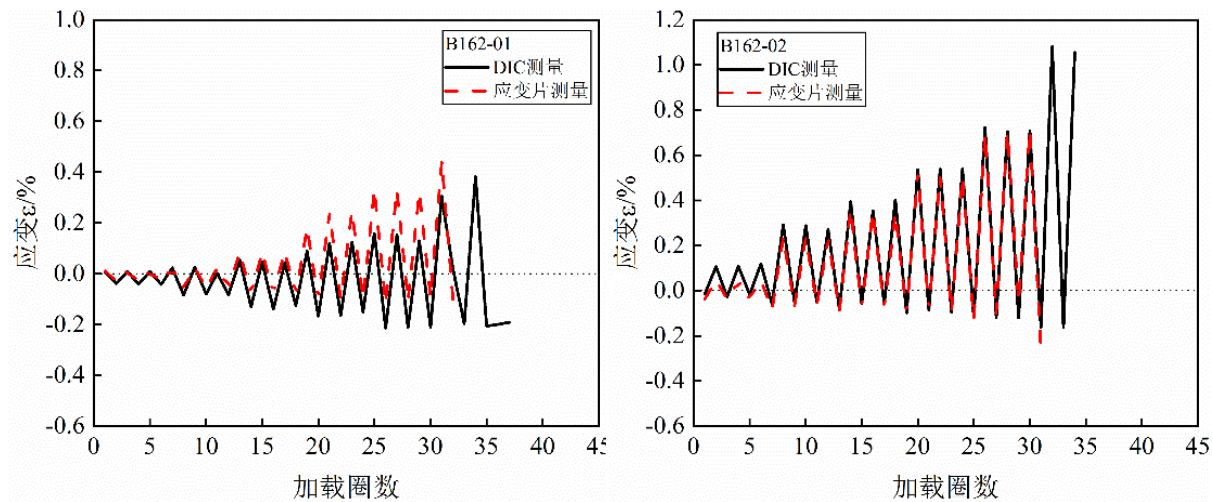


CS-reinforced pier
Reinforcement ratio: 1.62 %,
axial load: 0.2

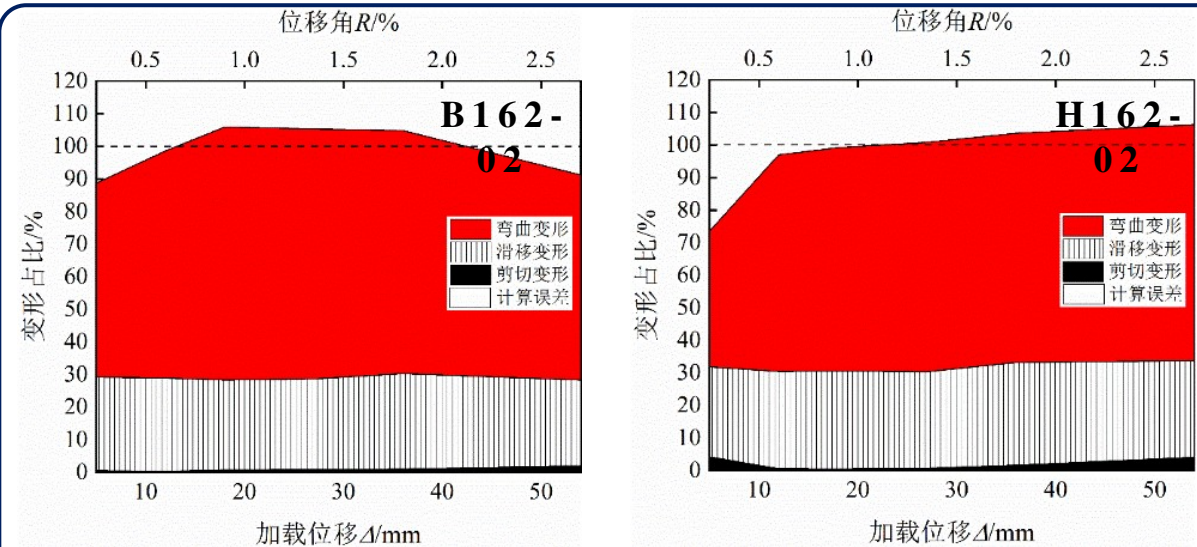
- With **the increase of axial compression ratio**, **the spalling height of concrete cover increases by approximately 5 %-20 %**.
- The spalling height of concrete cover in SS-reinforced concrete piers is **20 %-30 % higher** than that in conventional piers.
- B162-02 exhibited **double-wave buckling** of longitudinal reinforcement during the test, which may be attributed to **the low bond strength** between stainless steel rebars and concrete.



2 Quasi-static tests of SS-reinforced piers



DIC vs strain gauge

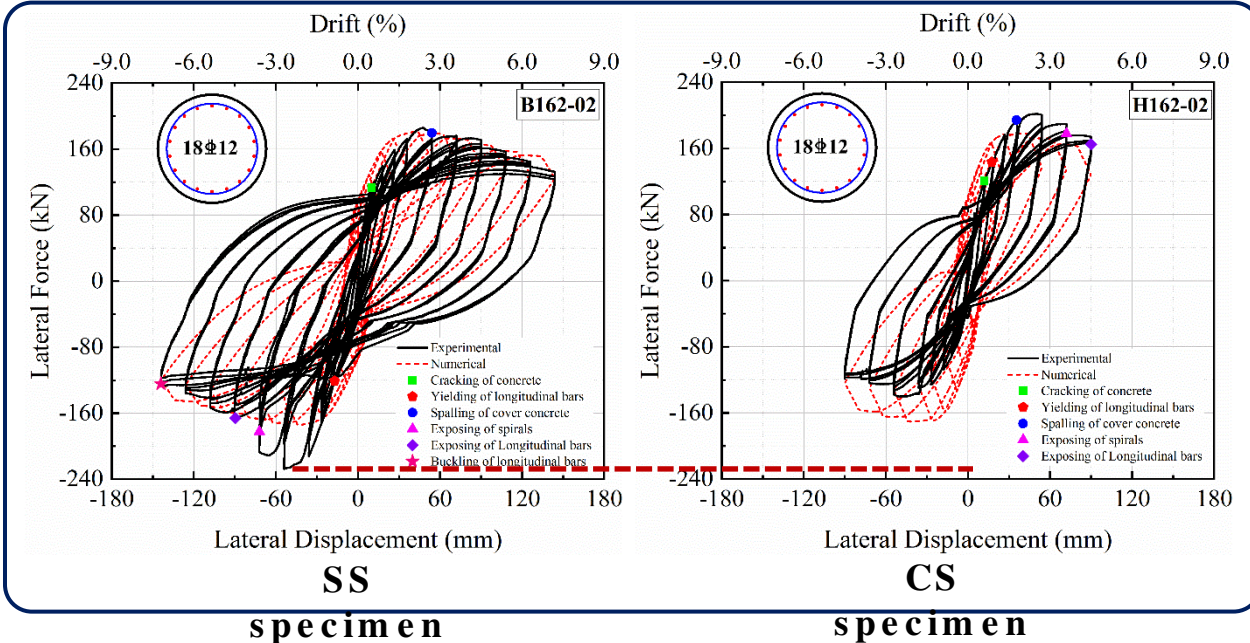
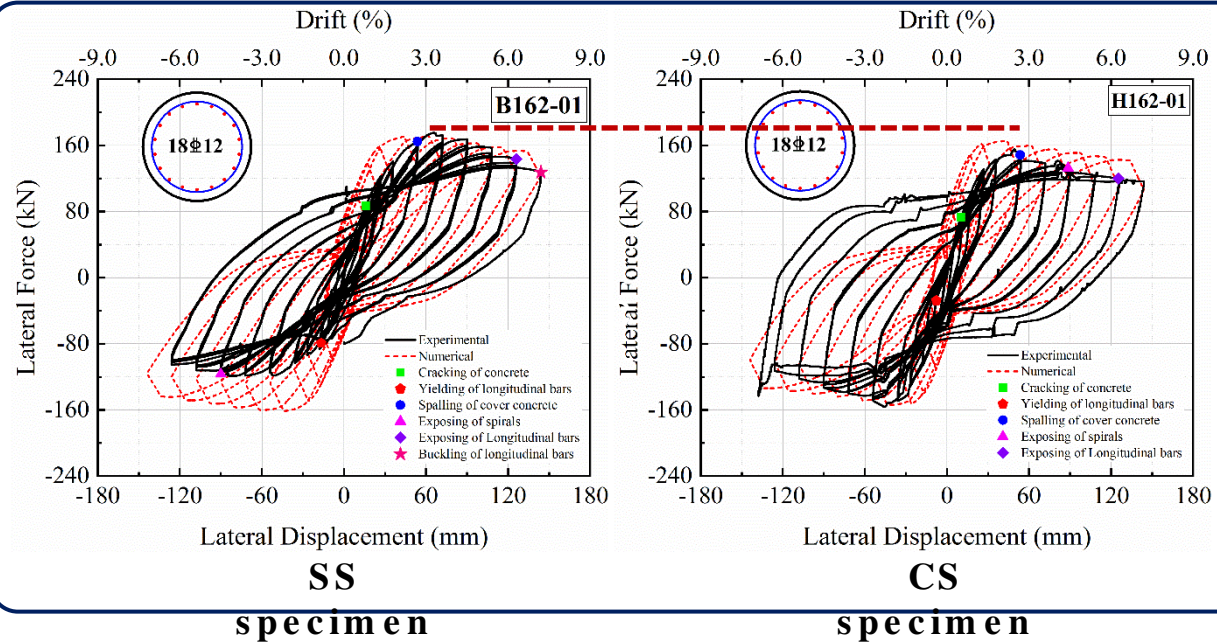


Deformation components

- Deformation components were calculated from **DIC-recorded data**.
- **Flexural deformation component** is 30%~50% in the early loading stage and increases to 70% in the later stage.
- **Slip deformation component** remained stable at 30%~40% throughout the loading process.
- Higher axial ratios **reduce** slip deformation.
- **Shear deformation** consistently accounted for less than 5% in all cases.



2 Quasi-static tests of SS-reinforced piers

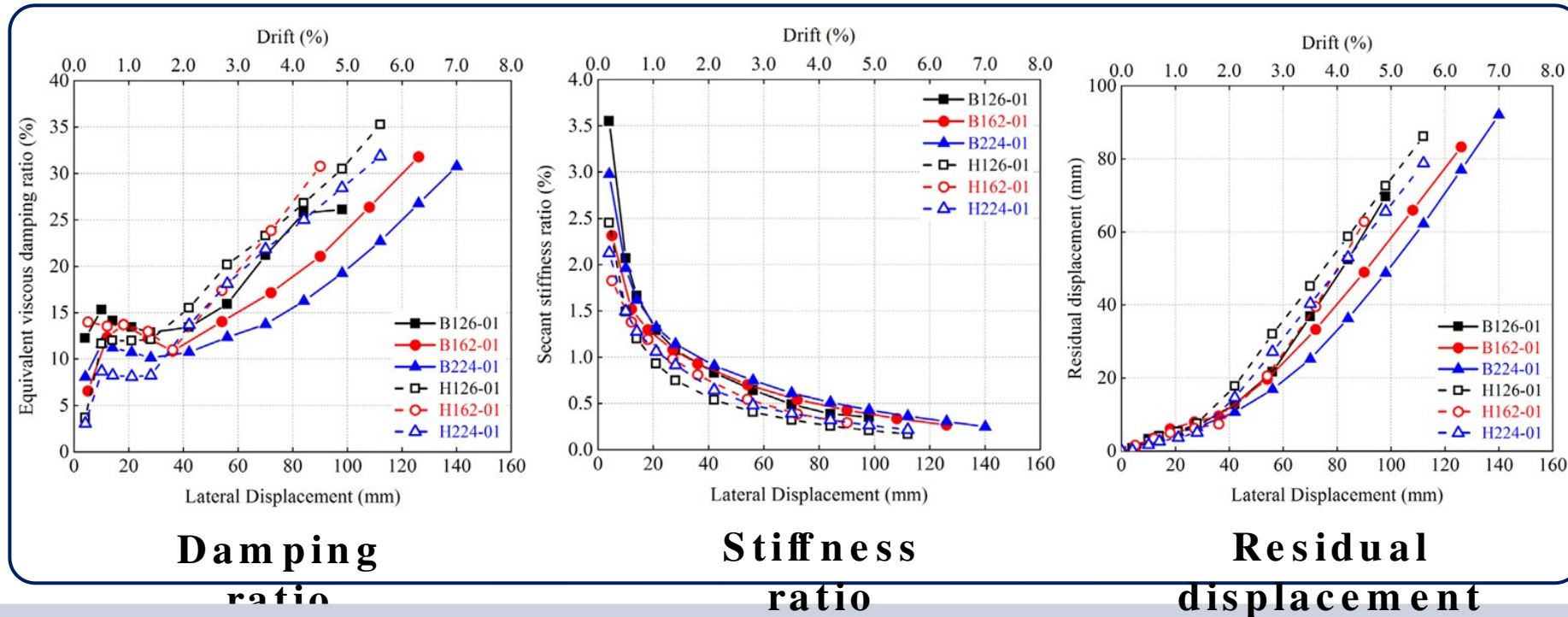


Under the same reinforcement arrangement:

- **CS piers exhibit fuller hysteresis curves**
- **SS piers show larger ultimate strength**



2 Quasi-static tests of SS-reinforced piers



For piers with identical design parameters:

- SS-reinforced piers exhibit **larger deformation capacity** compared to conventional piers, with maximum drift ratios exceeding 5% in all cases
- The **damping ratio** of SS-reinforced piers is **slightly lower** than that of conventional piers. However, SS specimen demonstrates **greater energy dissipation potential**
- SS-reinforced piers show **higher initial stiffness** than conventional counterparts
- **Stiffness degradation** occurs at a slower rate in SS-reinforced piers
- **Residual displacements** are consistently smaller in SS-reinforced piers

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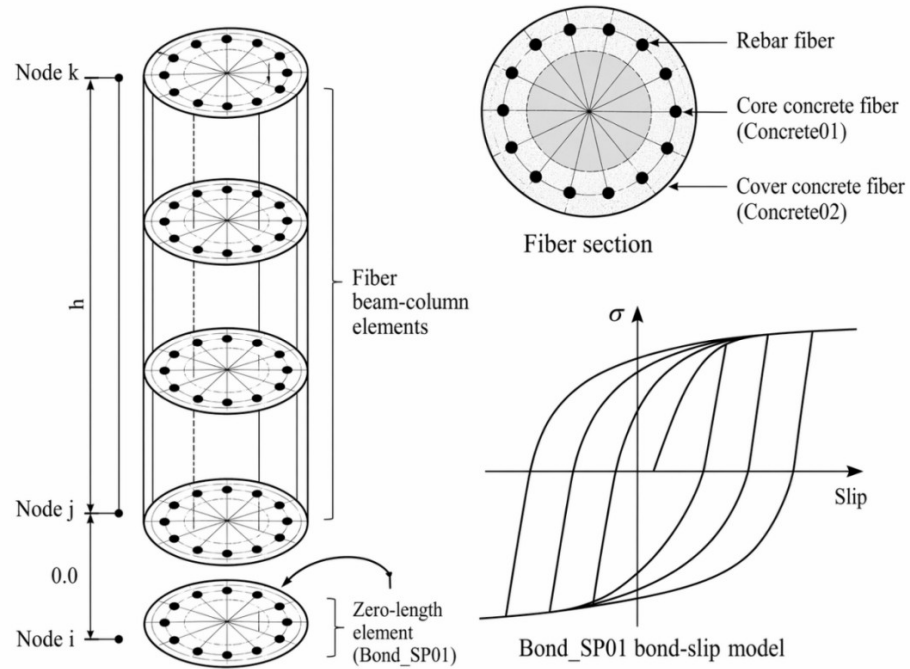
Numerical Modelling of SS-reinforced piers

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Plastic hinge model of SS-reinforced piers

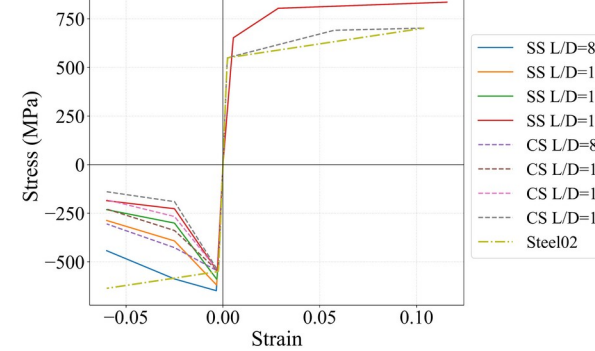
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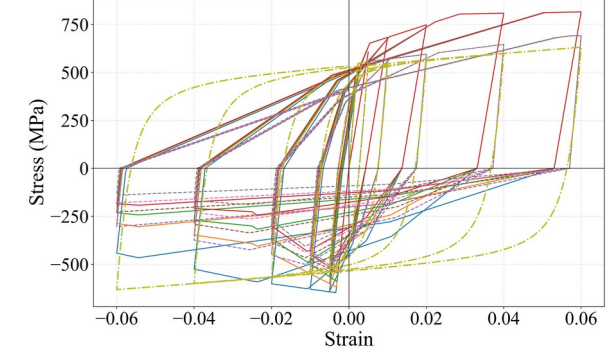


**Numerical model
established by
OpenSees**

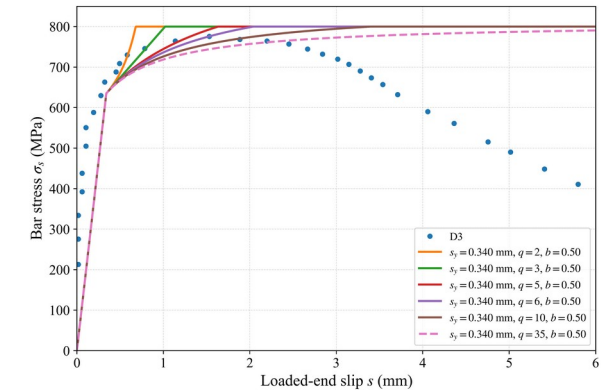
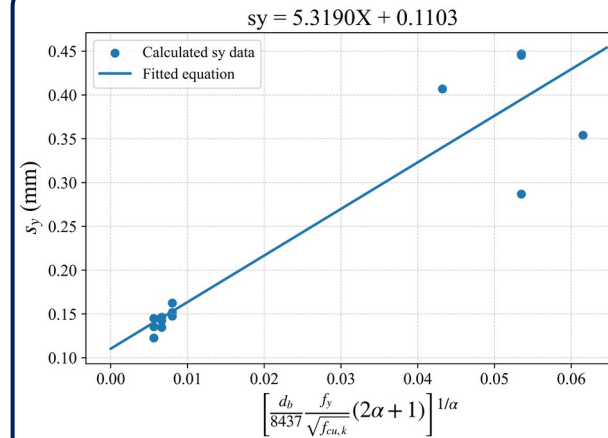
Raw Backbone Curves of All Groups



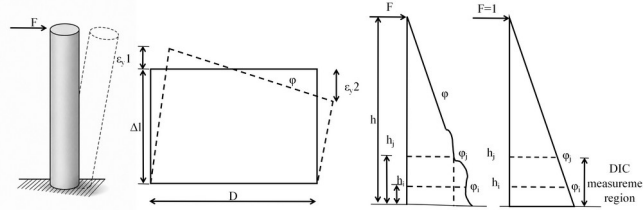
Cyclic Response of All Groups



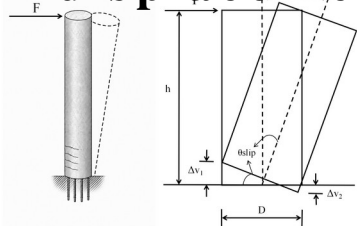
Inelastic buckling



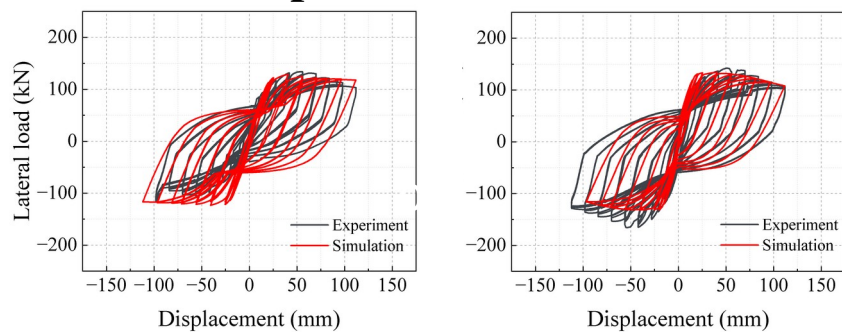
Bond slip effects



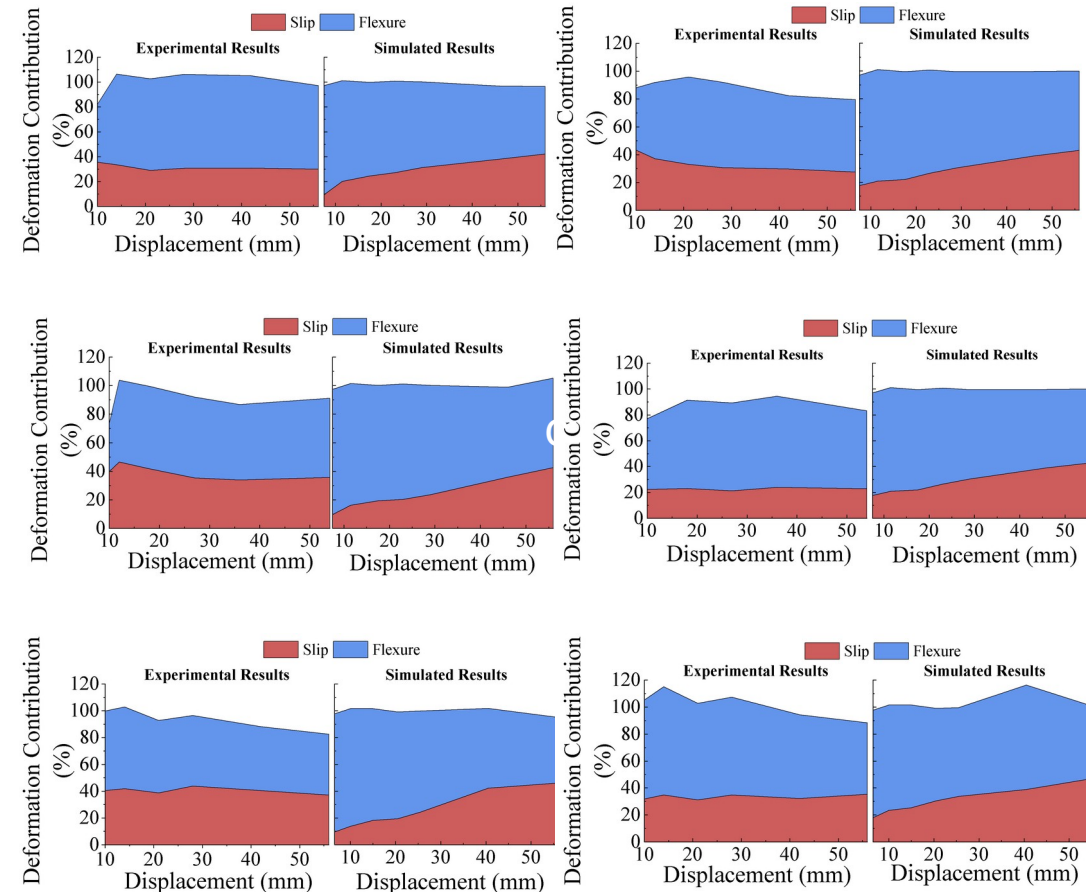
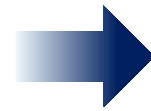
**Flexural
displacement**



**Slip
displacement**



**Hysteresis
behaviour**



**Displacement component
validation**

➤ The **global responses** and **displacement components** are in agreement with

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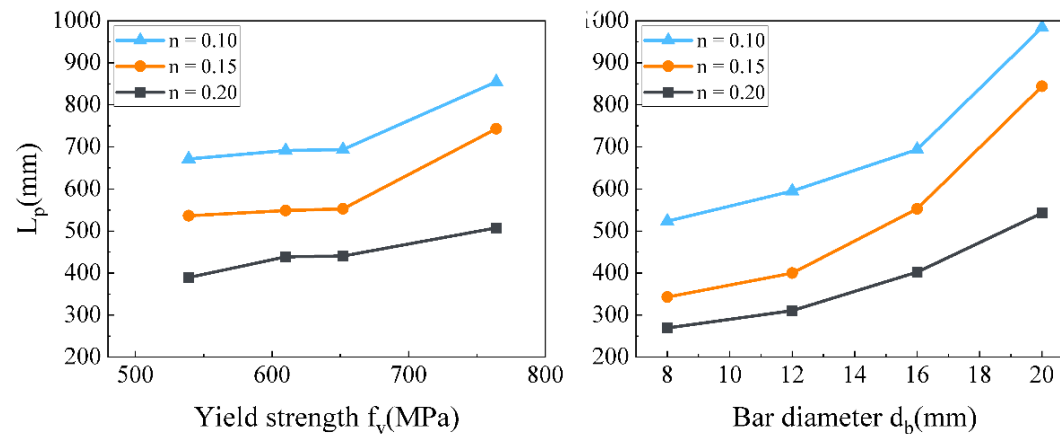
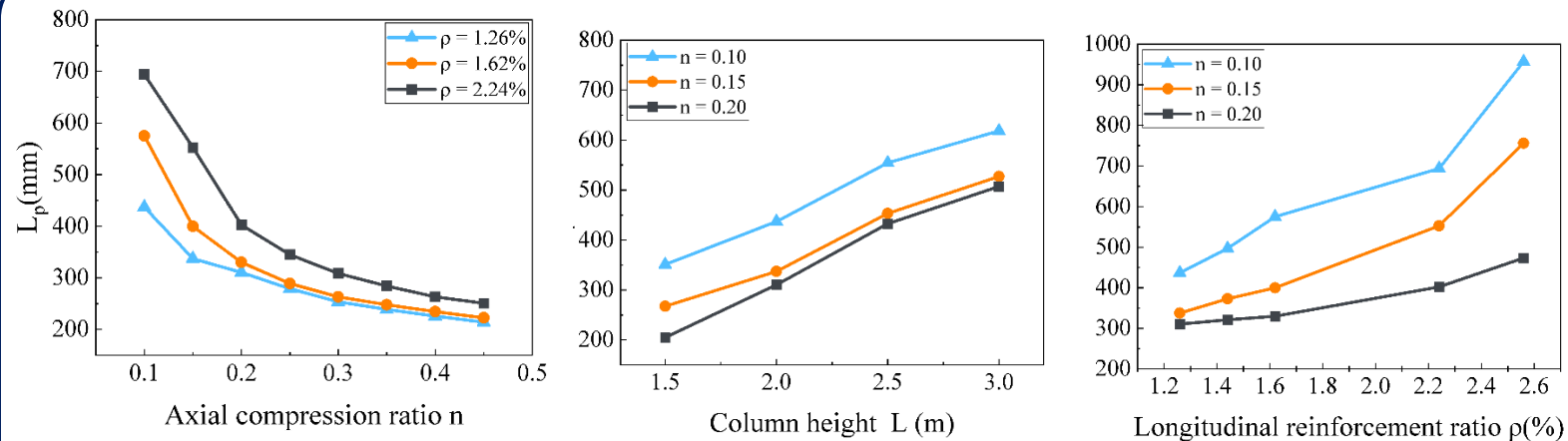
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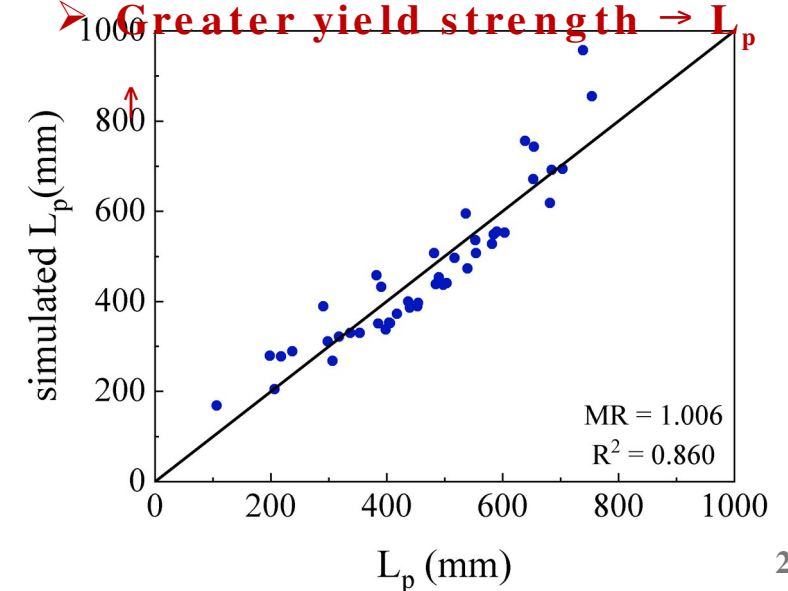
Parametric study

$$L_p = -1998.32n + 108.00\rho + 0.18403L + 0.02816(f_y d_b)$$

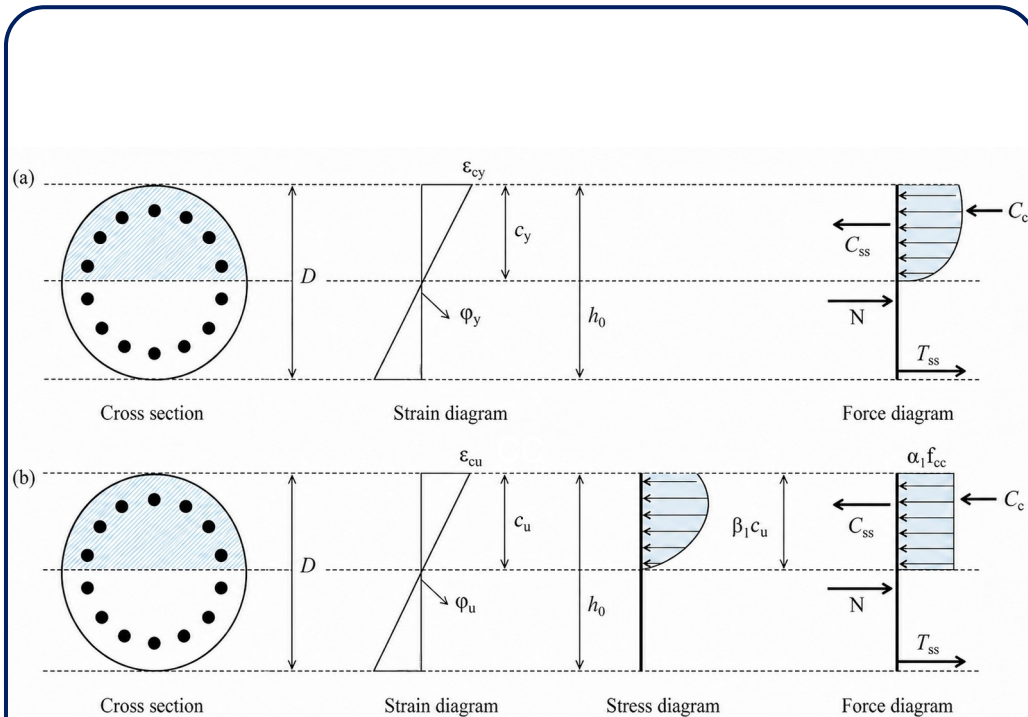
validation

- Axial load increases $\rightarrow L_p \downarrow$
- Greater column height $\rightarrow L_p \uparrow$
- Greater reinforcement ratio $\rightarrow L_p \uparrow$

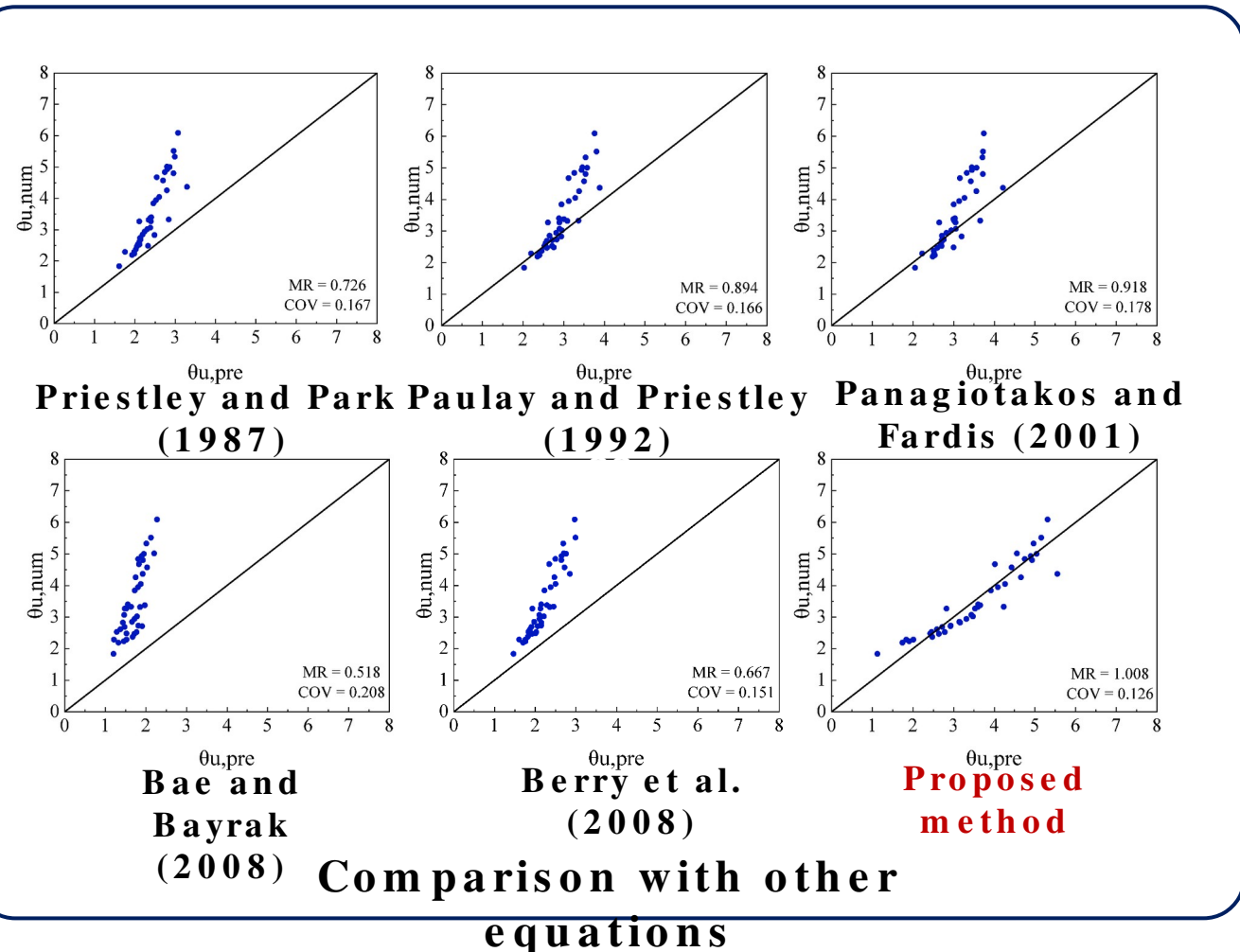
- Greater bar diameter $\rightarrow L_p \uparrow$
- Greater yield strength $\rightarrow L_p \uparrow$



Plastic hinge prediction of SS-reinforced piers



Cross-sectional strain and stress distributions



- Proposed L_p equation applied to predict pier ultimate deformation & compared with existing models.
- Our predictions match numerical simulations better than other empirical formulas.

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- SS-reinforced piers exhibit **larger ultimate strength**, **deformation capacity** (drift > 5%), and **initial stiffness**, with **slower stiffness degradation** and **smaller residual displacements** than conventional CS piers.
- **Flexural deformation** dominates (70% in later stage), slip deformation remains 30–40% (reduced by higher axial load), and shear deformation is negligible (< 5%).
- The OpenSees numerical model, incorporating **inelastic buckling** and **bond-slip effects**, accurately reproduces global responses and displacement components.
- Proposed L_p equation: L_p decreases with higher axial load; increases with column height, reinforcement ratio, bar diameter, and yield strength. It predicts **ultimate deformation** better than existing models.



**Thanks for your
attention!**